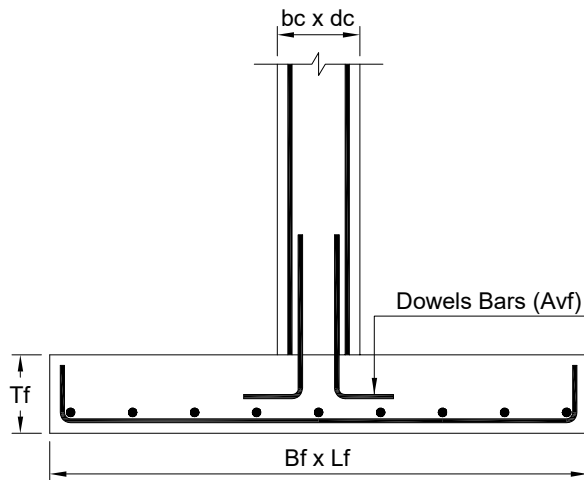




Design for Transfer of Horizontal Force at Base of Column where The Footing Surface is not Intentionally Roughened as per ACI 318-11 Chapter 12



System

| | |
|----------------------------|---------|
| Column Width, b_c = | 12.0 in |
| Column Depth, d_c = | 12.0 in |
| Footing Width, B_f = | 9.0 ft |
| Footing Length, L_f = | 9.0 ft |
| Footing Thickness, T_f = | 22.0 in |

Load

| | |
|--|-----------|
| Ultimate Horizontal Force at the Base of Column, V_u = | 84.0 kips |
|--|-----------|

Material Properties

| | |
|---|-----------|
| Concrete Strength, f'_c = | 4000 psi |
| Yield Strength of Reinforcement, f_y = | 60000 psi |
| Shear Strength Reduction Factor (According to Cl.9.3.2 of ACI318), Φ = | 0.75 |
| Modification Factor for Lightweight Concrete, λ = | 1.00 |
| Friction Factor (According to Cl.11.6.4.3 of ACI318), $\mu = 0.6 * \lambda$ | = 0.60 |

Check on Maximum Shear Transfer Permitted

| | | | |
|---|--|---|----------------------|
| Nominal Shear Force (According to Cl.11.6.5 of ACI318), | | | |
| ΦV_{n1} = | $\Phi * (0.2 * f'_c / 1000 * b_c * d_c)$ | = | 86.4 kips |
| ΦV_{n2} = | $\Phi * (800 * b_c * d_c) / 1000$ | = | 86.4 kips |
| Minimum Nominal Shear, ΦV_n = | $\text{MIN}(\Phi V_{n1}; \Phi V_{n2};)$ | = | 86.4 kips |
| Check Validity= | $\text{IF}(V_u < \Phi V_n; \text{"Valid"}; \text{"Increase Dimension"})$ | = | Valid |
| Required Area of Reinforcement (According to Eq.11-25 of ACI318), | | | |
| A_{vf} = | $\frac{V_u * 1000}{\Phi * f_y * \mu}$ | = | 3.11 in ² |



| | | | |
|--|---|---|----------------------|
| Provided Shear Reinforcement, Bar= | SEL("ACI/Bar"; Bar;) | = | No.8 |
| Diameter of Bars, Dia= | TAB("ACI/Bar"; Dia; Bar=Bar) | = | 1.0000 in |
| Number of Bars, n= | | | 4 |
| Provided Area of Reinforcement, A _s = | $n * \frac{\pi * Dia^2}{4}$ | = | 3.14 in ² |
| Check Validity= | IF(A _s >A _{vf} ; "Valid"; "Increase RFT") | = | Valid |

Check on Development Length of Tensile Reinforcement with Column

| | | | |
|---|-------------------|---|---------|
| Clear Cover to Center of Bars, c= | | | 3.25 in |
| Center to Center Bar Spacing, S= | | | 4.50 in |
| Factor of, cb= | MIN(c+Dia/2; S/2) | = | 2.25 in |
| (According to Cl.12.2.3 of ACI318) Factor of, K _{tr} = | | | 0.00 |
| (According to Cl.12.2.4 of ACI318) Factor of, Ψ _t = | | | 1.00 |
| (According to Cl.12.2.4 of ACI318) Factor of, Ψ _e = | | | 1.00 |
| (According to Cl.12.2.4 of ACI318) Factor of, Ψ _s = | | | 1.00 |

Development Length within Column

Development Length (According to Eq.12-1 of ACI318),

$$L_{d1} = \frac{3}{40} * \frac{f_y}{\lambda * \sqrt{f_c}} * \frac{\Psi_t * \Psi_e * \Psi_s}{(cb + K_{tr}) / Dia} * Dia = 31.6 \text{ in}$$

Development Length within Footing

Development Length (According to Cl.12.5.2 of ACI318),

$$L_{d2} = \frac{0.02 * \Psi_e * f_y}{\lambda * \sqrt{f_c}} * Dia = 19.0 \text{ in}$$

Design Summary

| | | | |
|--|-----------------|---|----------------------|
| Provided Area of Reinforcement, A _s = | A _s | = | 3.14 in ² |
| Development Length within Column, L _{d1} = | L _{d1} | = | 31.6 in |
| Development Length within Footing, L _{d2} = | L _{d2} | = | 19.0 in |