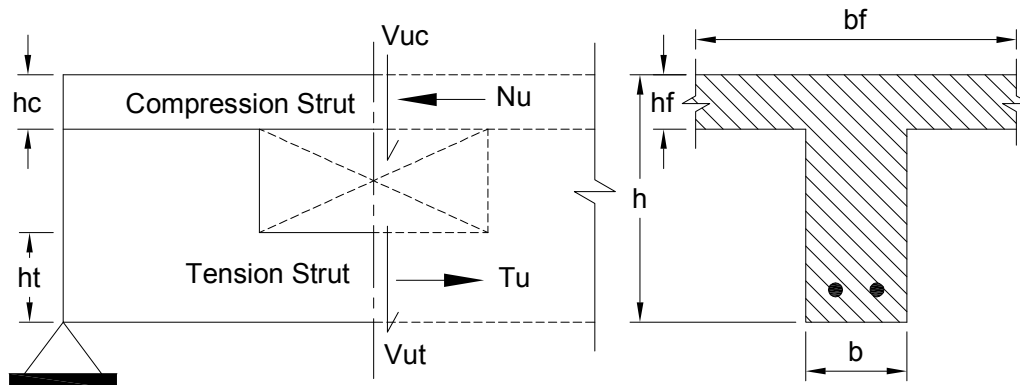


**Check Shear Reinforcement at Opening as per ACI 318-11 Chapter 11****System**

Width of Beam, b =	4.3 in
Width of Top Flange, b_f =	48.0 in
Height of Beam, h =	26.0 in
Height of Compression Strut, h_c =	4.0 in
Height of Tension Strut, h_t =	12.0 in

Load

Ultimate Shear Force at Center of Opening, V_u =	7.2 kips
Ultimate Axial Tension Force in Tension Strut, T_u =	-10.8 kips
Ultimate Axial Compression Force in Compression Strut, N_u =	60.0 kips
Ultimate Shear Force in Tension Strut, V_{ut} =	6.0 kips
Ultimate Shear Force in Compression Strut, V_{uc} =	5.4 kips

Material Properties

Concrete Strength for Beam, f'_{c1} =	6000 psi
Concrete Strength for Topping, f'_{c2} =	3000 psi
Yield Strength of Reinforcement, f_y =	60000 psi
Shear Strength Reduction Factor (According to Cl.9.3.2 of ACI318), Φ =	0.75
Modification Factor for Lightweight Concrete, λ =	1.00

Calculation of Required Shear Reinforcement

Required Shear RFT, A_{v_Req} =	$\frac{V_u}{\Phi * f_y / 1000}$	=	0.16 in ²
Identification of, Bar=	SEL("ACI/Bar" ;Bar;)	=	No.3
Provided Reinforcement, A_{sb} =	TAB("ACI/Bar"; Asb; Bar=Bar)	=	0.11 in ²
Number of Bars, n =			2
Provided Shear Reinforcement, A_{v_Prov} = $n * A_{sb}$		=	0.22 in ²
Check Validity=	IF($A_{v_Prov} \geq A_{v_Req}$; "Valid"; "Invalid")	=	Valid

**Calculation of Shear Reinforcement of Tensile Strut**

$$\text{Strut Depth, } d_t = 0.8 * h_t = 9.6 \text{ in}$$

Concrete Shear Strength for Tensile Strut (According to Eq.11-8 of ACI318),

$$V_{ct} = 2 * \left(1 + \frac{T_u * 1000}{500 * b * h_t} \right) * \lambda * \frac{\sqrt{f_{c1}}}{1000} * b * d_t = 3.72 \text{ kips}$$

$$\text{Shear Reinforcement for Ten. Strut} = \text{IF}(V_{ut} \leq \Phi * V_{ct}, \text{"Not Required"}, \text{"Required"}) = \text{Required}$$

Spacing between Stirrups (According to Cl.11.4.5.1 of ACI318),

$$s = 0.75 * h_t = 9.00 \text{ in}$$

$$\text{Required RFT Area, } A_{vt_Req} = \frac{(V_{ut} - \Phi * V_{ct}) * s}{\Phi * f_y * d_t / 1000} = 0.07 \text{ in}^2$$

$$\text{Identification of, Bar} = \text{SEL}(\text{"ACI/Bar"}; \text{Bar};) = \text{No.3}$$

$$\text{Provided Reinforcement, } A_{sb} = \text{TAB}(\text{"ACI/Bar"}; \text{Asb}; \text{Bar}=\text{Bar}) = 0.11 \text{ in}^2$$

$$\text{Number of Bars, } n = 1$$

$$\text{Provided Shear Reinforcement, } A_{vt_Prov} = n * A_{sb} = 0.11 \text{ in}^2$$

$$\text{Check Validity} = \text{IF}(A_{vt_Prov} \geq A_{vt_Req}; \text{"Valid"}, \text{"Invalid"}) = \text{Valid}$$

Calculation of Shear Reinforcement of Compression Strut

$$\text{Strut Depth, } d_c = 0.8 * h_c = 3.2 \text{ in}$$

Concrete Shear Strength for Tensile Strut (According to Eq.11-8 of ACI318),

$$V_{cc} = 2 * \left(1 + \frac{N_u * 1000}{2000 * b_f * h_c} \right) * \lambda * \frac{\sqrt{f_{c2}}}{1000} * b_f * d_c = 19.46 \text{ kips}$$

$$\text{Shear Reinforcement for Comp. Strut} = \text{IF}(V_{uc} \leq \Phi * V_{cc}, \text{"Not Required"}, \text{"Required"}) = \text{Not Required}$$

Spacing between Stirrups (According to Cl.11.4.5.1 of ACI318),

$$s = 0.75 * h_c = 3.00 \text{ in}$$

$$\text{Required RFT Area, } A_{vc_Req} = \frac{(V_{uc} - \Phi * V_{cc}) * s}{\Phi * f_y * d_c / 1000} = -0.19 \text{ in}^2$$

$$\text{Identification of, Bar} = \text{SEL}(\text{"ACI/Bar"}; \text{Bar};) = \text{No.3}$$

$$\text{Provided Reinforcement, } A_{sb} = \text{TAB}(\text{"ACI/Bar"}; \text{Asb}; \text{Bar}=\text{Bar}) = 0.11 \text{ in}^2$$

$$\text{Number of Bars, } n = 1$$

$$\text{Provided Shear Reinforcement, } A_{vc_Prov} = n * A_{sb} = 0.11 \text{ in}^2$$

$$\text{Check Validity} = \text{IF}(A_{vc_Prov} \geq A_{vc_Req}; \text{"Valid"}, \text{"Invalid"}) = \text{Valid}$$

Design Summary

$$\text{Shear Reinforcement for Beam, } A_{v_Prov} = A_{v_Prov} = 0.22 \text{ in}$$

$$\text{Shear Reinforcement for Ten. Strut, } A_{vt_Prov} = \text{IF}(V_{ut} \leq \Phi * V_{ct}, \text{"Zero"}; A_{vt_Prov}) = 0.11 \text{ in}^2$$

$$\text{Shear Reinforcement for Com. Strut, } A_{vc_Prov} = \text{IF}(V_{uc} \leq \Phi * V_{cc}, \text{"Zero"}; A_{vc_Prov}) = \text{Zero}$$